
Added Resistance by means of time-domain models in seakeeping



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Non-linear formulation

Potential theory

$$\Delta\Phi = 0$$

Free-surface condition (no surface tension) on $z = \zeta(x, y)$

$$g\frac{\partial\Phi}{\partial z} + \frac{\partial^2\Phi}{\partial t^2} + \nabla\Phi \cdot \nabla\frac{\partial\Phi}{\partial t} + \left(\frac{\partial\Phi}{\partial x}\frac{\partial}{\partial x_\zeta} + \frac{\partial\Phi}{\partial y}\frac{\partial}{\partial y_\zeta}\right) \left(\frac{\partial\Phi}{\partial t} + \frac{1}{2}\nabla\Phi \cdot \nabla\Phi\right) = 0$$

where

$$\frac{\partial F(x, y, \zeta(x, y))}{\partial x_\zeta} = \frac{\partial F}{\partial x} + \frac{\partial F}{\partial z} \frac{\partial \zeta}{\partial x}$$

is differentiation along the free-surface.

At the exact hull $H(t)$ we have

$$\frac{\partial \Phi}{\partial n} = \frac{\partial \boldsymbol{\alpha}}{\partial t} \cdot \mathbf{n},$$

where $\boldsymbol{\alpha}$ is the displacement in the mean ship-fixed coordinate system.

Radiation condition.

Decomposition of the potential

We decompose the potential function in a steady and unsteady part

$$\Phi(\mathbf{x}, t) = \Phi_s(\mathbf{x}) + \phi_u(\mathbf{x}, t).$$

Choices for the steady part are

- $\Phi_s(\mathbf{x}) = Ux$ the unperturbed flow
- $\Phi_s(\mathbf{x}) = \Phi_r(\mathbf{x})$ double body flow
- $\Phi_s(\mathbf{x}) = \Phi_r(\mathbf{x}) + \phi(\mathbf{x})$
- Solution of the nonlinear steady problem (RAPID)

The steady potential

The non-linear free surface conditions for the steady potential are

$$\frac{\partial \Phi_s}{\partial x} \frac{\partial \zeta_s}{\partial x} + \frac{\partial \Phi_s}{\partial y} \frac{\partial \zeta_s}{\partial y} - \frac{\partial \Phi_s}{\partial z} = 0 \quad \text{on } z = \zeta_s,$$

ζ_s is the steady free-surface elevation that satisfies

$$\zeta_s = -\frac{1}{2g} (\nabla \Phi_s \cdot \nabla \Phi_s - U^2).$$

with $\Phi_s(\mathbf{x}) = \Phi_r(\mathbf{x}) + \phi(\mathbf{x})$ and $z' = z - \zeta_r$ the free surface condition becomes

$$\begin{aligned} \phi_z + \frac{1}{g} [& \Phi_{rx}^2 \phi_{xx} + 2\Phi_{rx} \Phi_{ry} \phi_{xy} + \Phi_{ry}^2 \phi_{yy} + \\ & (3\Phi_{rx} \Phi_{rxx} + 2\Phi_{ry} \Phi_{rxy} + \Phi_{rx} \Phi_{rzz}) \phi_x + \\ & (3\Phi_{ry} \Phi_{ryy} + 2\Phi_{rx} \Phi_{rxy} + \Phi_{ry} \Phi_{rxx}) \phi_y] = D(x, y) \quad \text{at } z = 0, \end{aligned}$$

The steady potential

with

$$D(x, y) = \frac{\partial}{\partial x} [\zeta_r(x, y) \Phi_{rx}(x, y, 0)] + \frac{\partial}{\partial y} [\zeta_r(x, y) \Phi_{ry}(x, y, 0)]$$

and

$$\zeta_r = \frac{1}{2g} [U^2 - \Phi_{rx}^2(x, y, 0) - \Phi_{ry}^2(x, y, 0)] .$$

The condition advocated by Dawson is

$$(\Phi_{rl}^2 \phi_l)_l + g \phi_z = 2 \Phi_{rl}^2 \Phi_{rll},$$

where l is a curvilinear coordinate along the streamlines of the double body flow.

Source distribution

$$\Phi_s(\mathbf{x}) = \Phi_\infty(\mathbf{x}) + \int \int_{\partial D} \sigma(\boldsymbol{\xi}) G(\boldsymbol{\xi}; \mathbf{x}) dS_\xi,$$

where for deep water the Green's function is chosen as

$$G(\boldsymbol{\xi}; \mathbf{x}) = -\frac{1}{4\pi r} \quad r = |\mathbf{x} - \boldsymbol{\xi}|.$$

The integration may be chosen along the ship hull and the actual free surface or raised panels.

Several sources of errors such as

- choice of difference schemes
- position of raised panels $y_{fs} = \alpha \Delta x$
- upstream shift of collocation points $\gamma \Delta x$
- × × ×

Dispersion ??

Introduce (notation: Sclavounos and Nakos)

$$s := \frac{k\Delta x}{2\pi} \quad F_{n\Delta} := \frac{U_\infty}{\sqrt{g\Delta x}}.$$

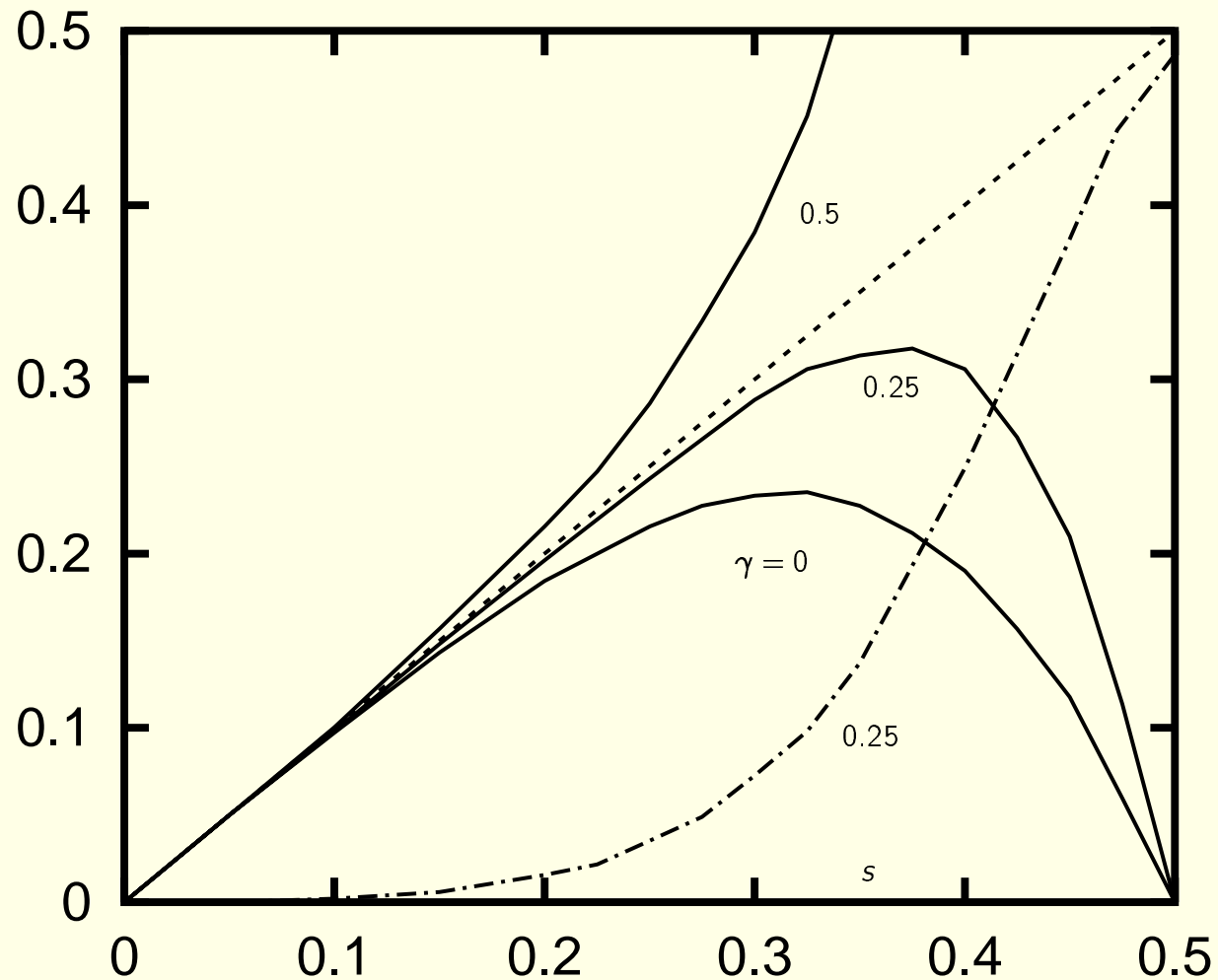
The continuous *dispersion* expression

$$\widetilde{\mathcal{W}}_\nu = k_0 - k = k_0(1 - 2\pi F n_\Delta^2 s).$$

The dispersion relation for the discrete operator becomes

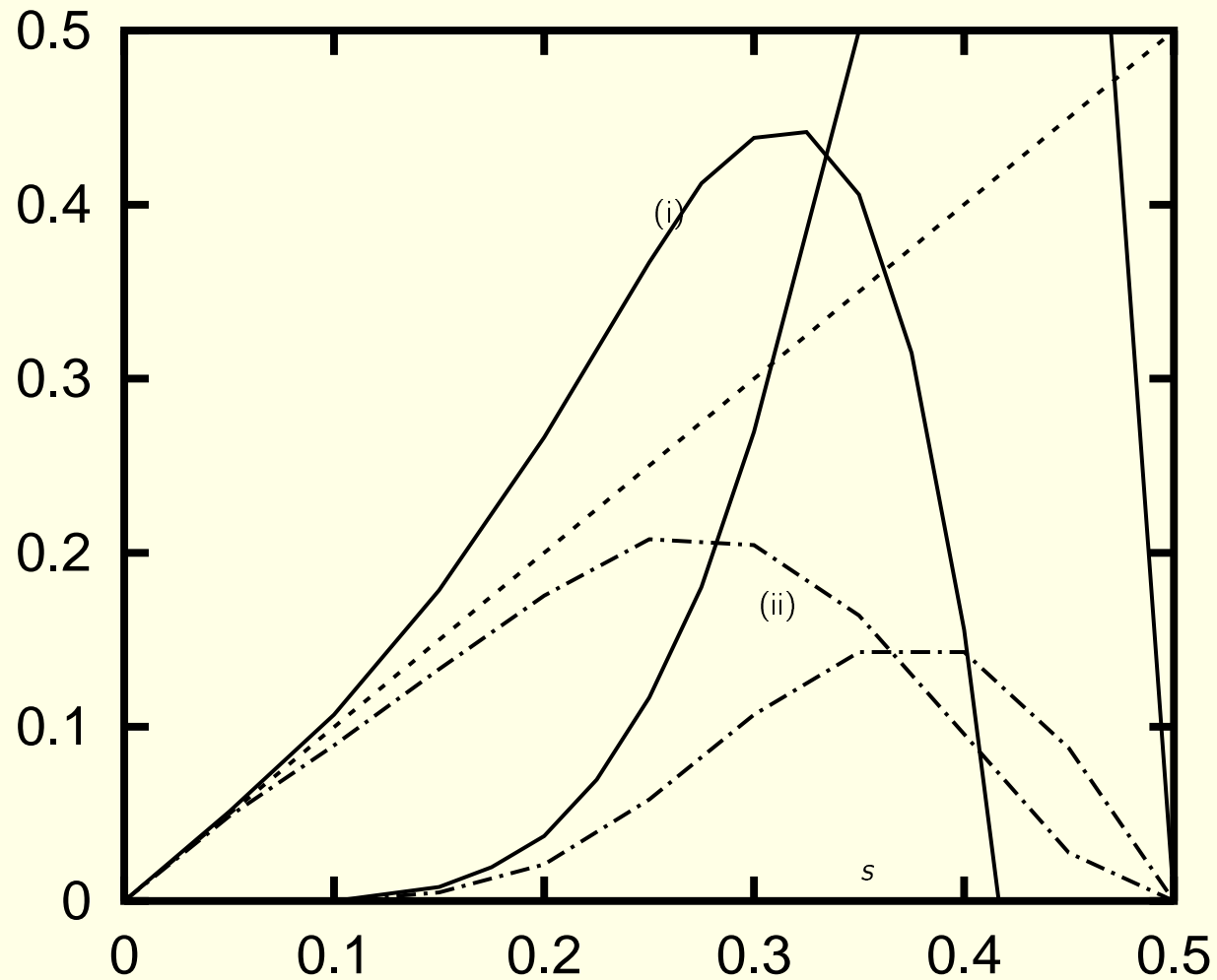
$$\widehat{\mathcal{W}}_\nu = k_0(1 - 2\pi F n_\Delta^2 L h(s)).$$

Deviation in the dispersion



$\Re Lh(s)$ for $\alpha = 0.5$ and $\gamma = 0.5, 0.25, 0$ and $\Im Lh(s)$ for $\gamma = 0.25$.

Deviation in the dispersion



\Re and $\Im Lh(s)$ (i) for $\alpha = 1$, $\gamma = 0.25$ and Dawson (ii).

We linearise along the steady free surface $z = \zeta_s$

$$\begin{aligned} & \frac{\partial^2 \phi_u}{\partial t^2} + 2 \nabla \Phi_s \cdot \nabla \frac{\partial \phi_u}{\partial t} + \nabla \Phi_s \cdot \nabla (\nabla \Phi_s \cdot \nabla \phi_u) + \\ & \frac{1}{2} \left(\frac{\partial \phi_u}{\partial x} \frac{\partial}{\partial x_{\zeta_s}} + \frac{\partial \phi_u}{\partial y} \frac{\partial}{\partial y_{\zeta_s}} \right) \|\nabla \Phi_s\|^2 + g \frac{\partial \phi_u}{\partial z} + \\ & \zeta_u \frac{\partial}{\partial z} \left(\frac{1}{2} \left(\frac{\partial \Phi_s}{\partial x} \frac{\partial}{\partial x_{\zeta_s}} + \frac{\partial \Phi_s}{\partial y} \frac{\partial}{\partial y_{\zeta_s}} \right) \|\nabla \Phi_s\|^2 + g \frac{\partial \Phi_s}{\partial z} \right) = 0. \end{aligned}$$

For $\Phi_s = Ux$

$$\frac{\partial^2 \phi_u}{\partial t^2} + 2U \frac{\partial^2 \phi_u}{\partial x \partial t} + U^2 \frac{\partial^2 \phi_u}{\partial x^2} + g \frac{\partial \phi_u}{\partial z} = 0 \quad \text{on } z = 0.$$

For $\Phi_s = \Phi_r(\mathbf{x})$, with $\mathbf{u} = (u, v, w) = \nabla \Phi_r(\mathbf{x})$ (Baba)

$$\frac{1}{g} \left[\frac{\partial}{\partial t} + u \frac{\partial}{\partial x} + v \frac{\partial}{\partial y} \right]^2 \phi + \frac{\partial}{\partial z} \phi = 0 \quad \text{on } z = 0,$$

Ray expansion

$$\phi(\mathbf{x}, t; k) = a(\mathbf{x}, k) e^{ikS(\mathbf{x}) - i\omega t},$$

$$a(\mathbf{x}, k) = \sum_{j=0}^N \frac{a_j(\mathbf{x})}{(ik)^j} + o((ik)^{-N}).$$

with $k = \omega^2/g$ and $\omega = \omega_0 + k_0 U \cos \theta$

Asymptotic formulation

Eikonal equation with $\mathbf{p} := (S_x, S_y)$

$$F(x, y, S, p, q) = (1 - \mathbf{u} \cdot \nabla S)^4 - \nabla S \cdot \nabla S = 0.$$

Transport equation

$$\{2\nabla S + 4(1 - \mathbf{u} \cdot \nabla S)^3 \mathbf{u}\} \cdot \nabla a_0 + a_0 MS = 0,$$

where

$$MS = \Delta_3 S - 2\mathbf{u} \cdot \nabla(\mathbf{u} \cdot \nabla S)(1 - \mathbf{u} \cdot \nabla S)^2.$$

Characteristic equations

$$\frac{dx}{d\sigma} = F_p = -4(1 - \mathbf{u} \cdot \mathbf{p})^3 u - 2p,$$

$$\frac{dy}{d\sigma} = F_p = -4(1 - \mathbf{u} \cdot \mathbf{p})^3 v - 2q,$$

$$\frac{dp}{d\sigma} = -(F_x + pF_S) = 4(1 - \mathbf{u} \cdot \mathbf{p})^3 (\mathbf{u}_x \cdot \mathbf{p}),$$

$$\frac{dq}{d\sigma} = -(F_y + qF_S) = 4(1 - \mathbf{u} \cdot \mathbf{p})^3 (\mathbf{u}_y \cdot \mathbf{p}).$$

and

$$\frac{dS}{d\sigma} = pF_p + qF_q = -4(1 - \mathbf{u} \cdot \mathbf{p})^3 + 2\mathbf{p} \cdot \mathbf{p}.$$

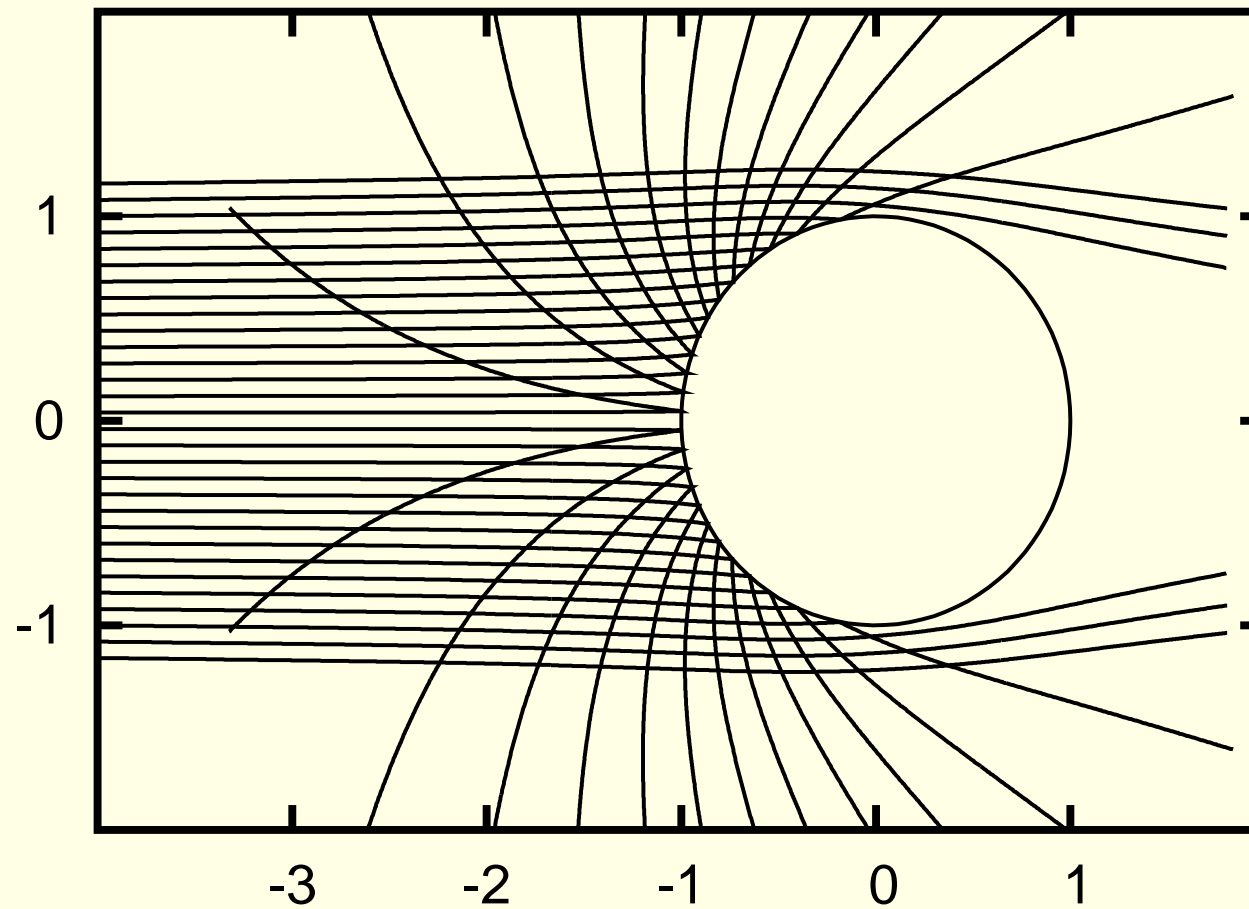
$$\frac{da_0}{d\sigma} = a_0 MS.$$

Characteristic equations

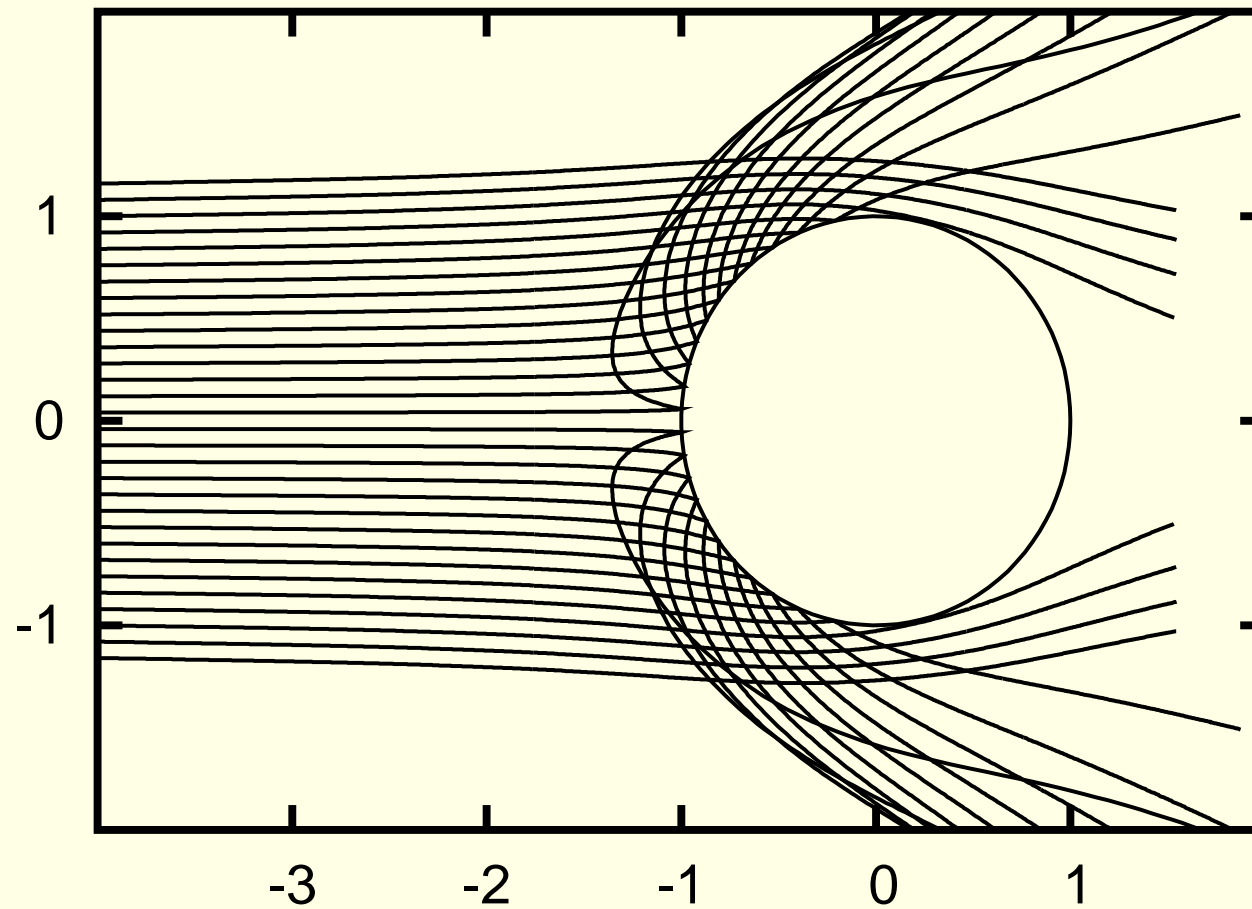
This operator MS has the final form

$$\begin{aligned} MS = & S_{xx} \left\{ 1 - 2|\nabla S|u^2 - \frac{S_x^2}{S_x^2 + S_y^2} \right\} + \\ & S_{xy} \left\{ -4|\nabla S|u^2 - 2\frac{S_x S_y}{S_x^2 + S_y^2} \right\} + \\ & S_{yy} \left\{ 1 - 2|\nabla S|u^2 - \frac{S_x^2}{S_x^2 + S_y^2} \right\} - 2|\nabla S|\nabla(\mathbf{u} \cdot \mathbf{u}) \cdot \nabla S. \end{aligned}$$

Ray pattern $\tau = 0.25$



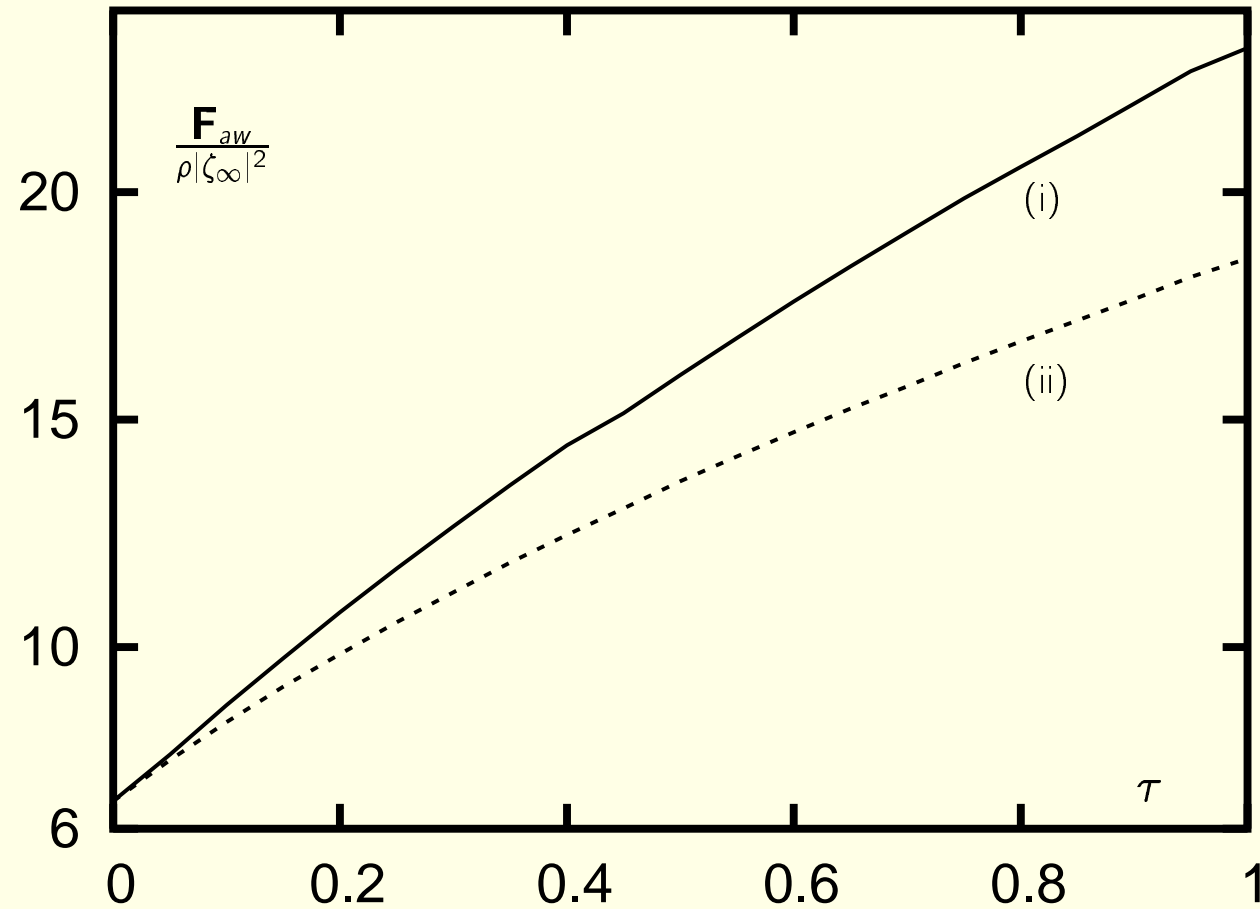
Ray pattern $\tau = 0.5$



Added resistance

$$\begin{aligned}\mathbf{F}_{aw} = & - \overline{\int_{z=-\infty}^{\zeta} \int_{WL} p \mathbf{n} dl dz} = \\ & - \frac{1}{4} \int_{WL} \left\{ \left(\nabla S^{(i)} \cdot \nabla S^{(i)} \right)^{\frac{1}{4}} a_0^{(i)} + \left(\nabla S^{(r)} \cdot \nabla S^{(r)} \right)^{\frac{1}{4}} a_0^{(r)} \right\}^2 \mathbf{n} dl \\ & + \frac{1}{4} \int_{WL} \left\{ a_0^{(i)2} |\nabla S^{(i)}| + a_0^{(r)2} |\nabla S^{(r)}| + \right. \\ & \left. 2 a_0^{(i)} a_0^{(r)} \frac{\nabla S^{(i)} \cdot \nabla S^{(r)} + |\nabla S^{(i)}| |\nabla S^{(r)}|}{|\nabla S^{(i)}| + |\nabla S^{(r)}|} \right\} \mathbf{n} dl.\end{aligned}$$

Added resistance for (i) a circular cylinder and (ii) a sphere



With time-step Δt we use the second order difference schemes:

$$\frac{\partial^2 \phi^i}{\partial t^2} = \frac{1}{(\Delta t)^2} (2\phi^i - 5\phi^{i-1} + 4\phi^{i-2} - \phi^{i-3}) + \mathcal{O}((\Delta t)^2)$$

$$\frac{\partial \phi^i}{\partial t} = \frac{1}{\Delta t} \left(\frac{3}{2}\phi^i - 2\phi^{i-1} + \frac{1}{2}\phi^{i-2} \right) + \mathcal{O}((\Delta t)^2)$$

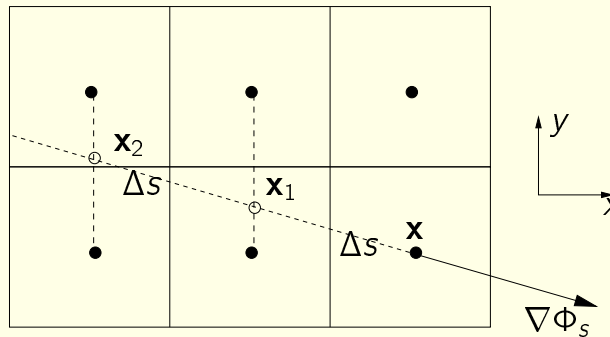
This leads to the following FSC

$$\begin{aligned}
 & \phi^i \left(\frac{2}{(\Delta t)^2} - \frac{T}{gS} \frac{3}{2\Delta t} \right) + \nabla \Phi_s \cdot \nabla (\nabla \Phi_s \cdot \nabla \phi^i) + \\
 & \quad \left(2 \frac{3}{2\Delta t} - \frac{T}{gS} \right) \nabla \phi^i \cdot \nabla \Phi_s + g \frac{\partial \phi^i}{\partial z} + \\
 & \quad \frac{1}{2} \left(\frac{\partial \phi^i}{\partial x} \frac{\partial}{\partial x_{\zeta_s}} + \frac{\partial \phi^i}{\partial y} \frac{\partial}{\partial y_{\zeta_s}} \right) \|\nabla \Phi_s\|^2 = f \quad \text{on } z = \zeta_s \\
 T &= \frac{\partial}{\partial z} \left(\frac{1}{2} \left(\frac{\partial \Phi_s}{\partial x} \frac{\partial}{\partial x_{\zeta}} + \frac{\partial \Phi_s}{\partial y} \frac{\partial}{\partial y_{\zeta}} \right) \|\nabla \Phi_s\|^2 + g \frac{\partial \Phi_s}{\partial z} \right) \quad \text{on } z = \zeta_s \\
 S &= 1 + \frac{1}{2g} \frac{\partial}{\partial z} \|\nabla \Phi_s\|^2 \\
 f &= \frac{5\phi^{i-1} - 4\phi^{i-2} + \phi^{i-3}}{(\Delta t)^2} + \left(2\nabla \Phi_s \cdot \nabla - \frac{T}{gS} \right) \frac{(2\phi^{i-1} - \frac{1}{2}\phi^{i-2})}{\Delta t}
 \end{aligned}$$

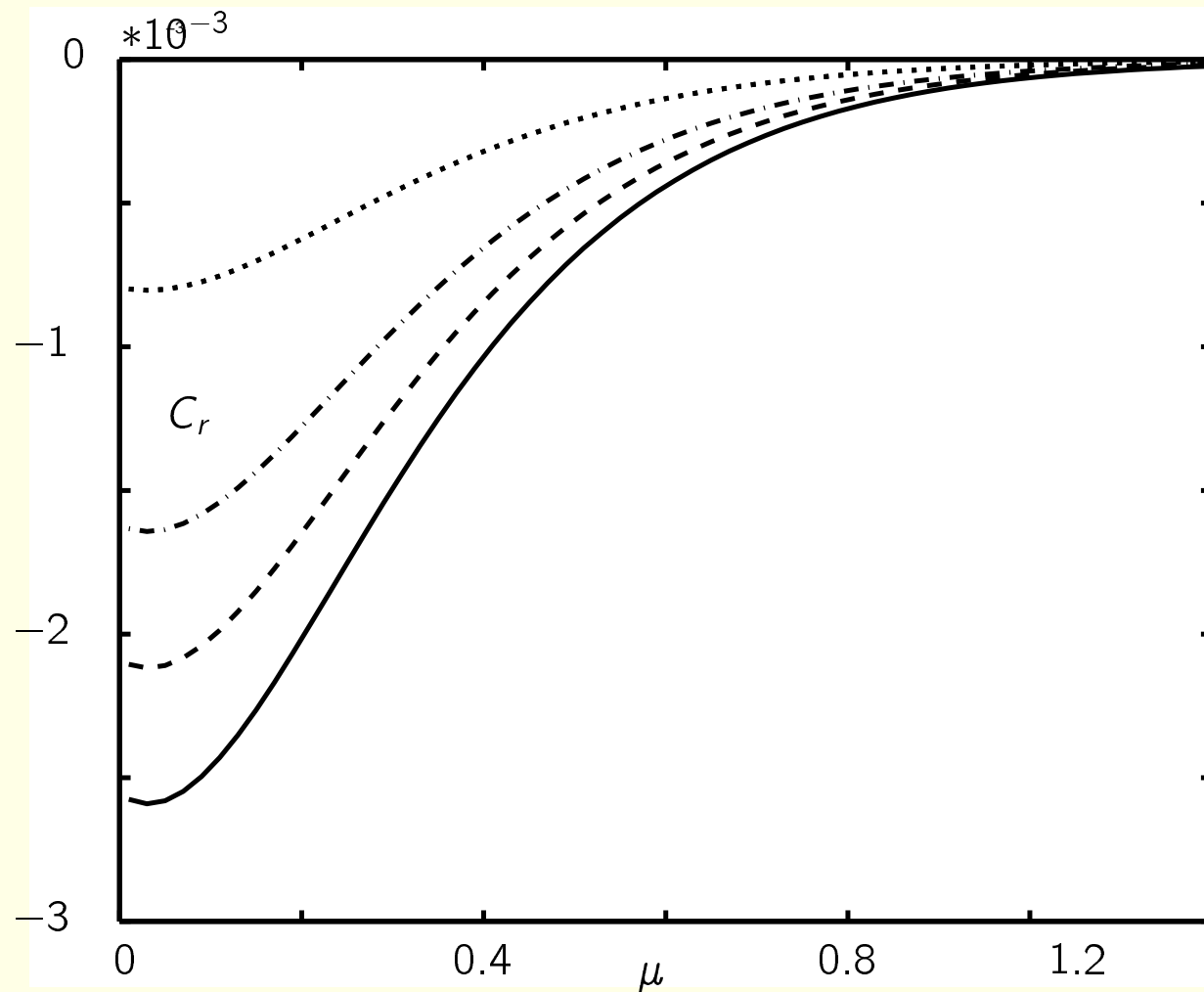
For example, we write

$$\nabla \Phi_s \cdot \nabla \phi = \|\nabla \Phi_s\| \frac{\frac{3}{2}\phi(\mathbf{x}) - 2\phi(\mathbf{x}_1) + \frac{1}{2}\phi(\mathbf{x}_2)}{\Delta s} + \mathcal{O}\left((\Delta s)^2\right)$$

difference scheme for $\nabla \Phi_s \cdot \nabla \phi$.

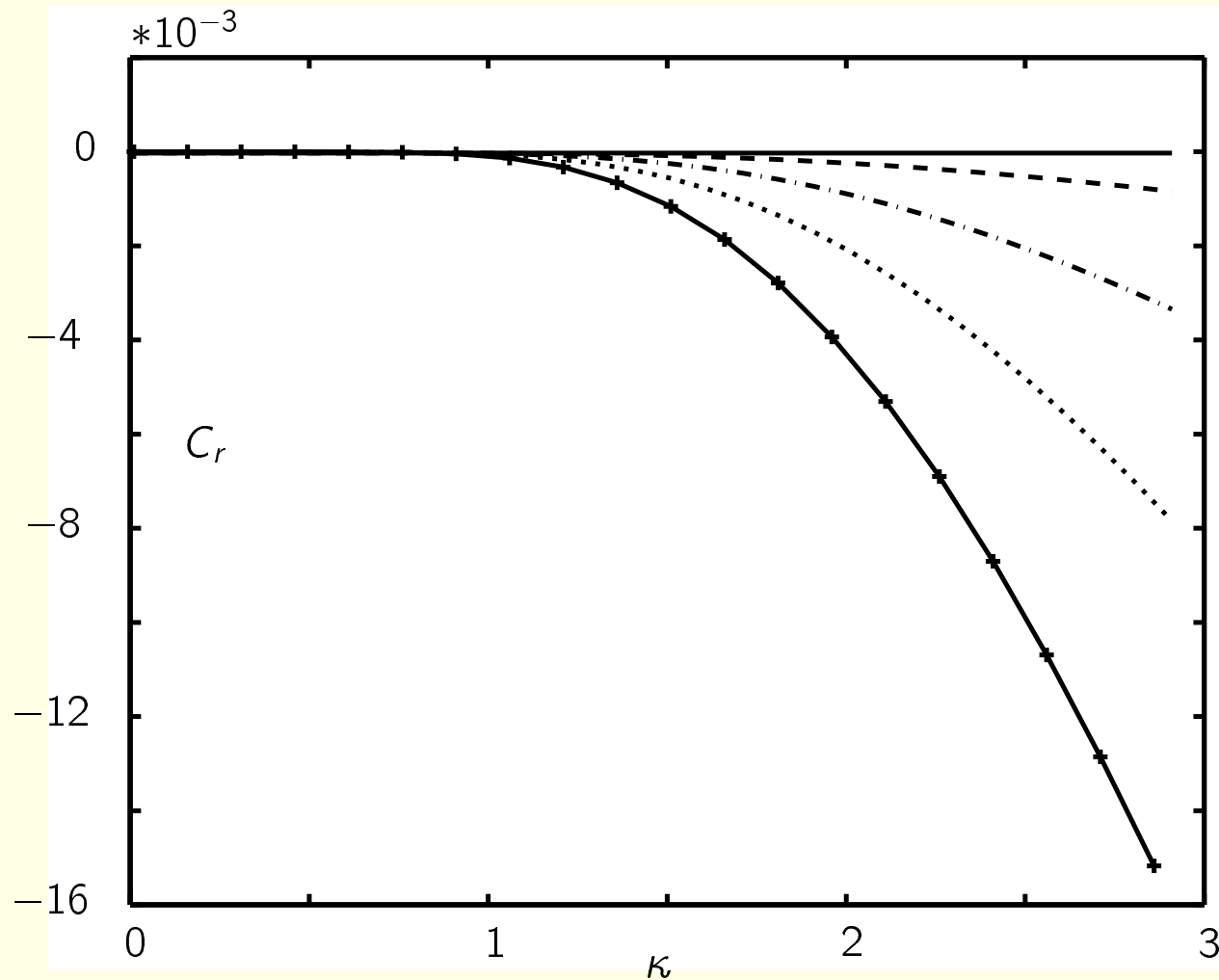


Deviation in the dispersion



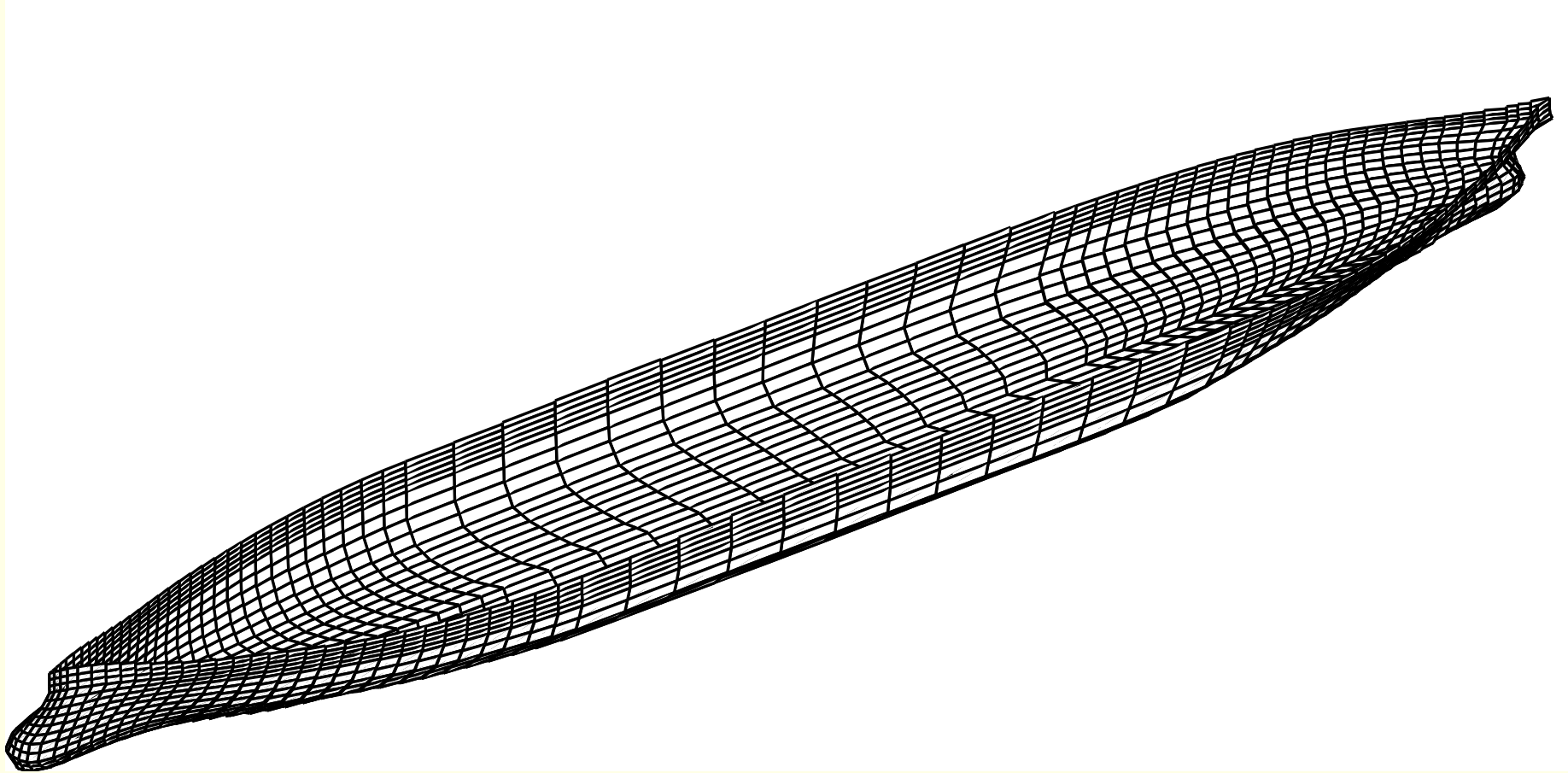
$\tau = 5, 1, 0.5, 0.25$ (top down), $Fn = 0.4$, $\theta = 0$, $\kappa = 1$, $\hat{\alpha} = 0.05$.

Deviation in the dispersion

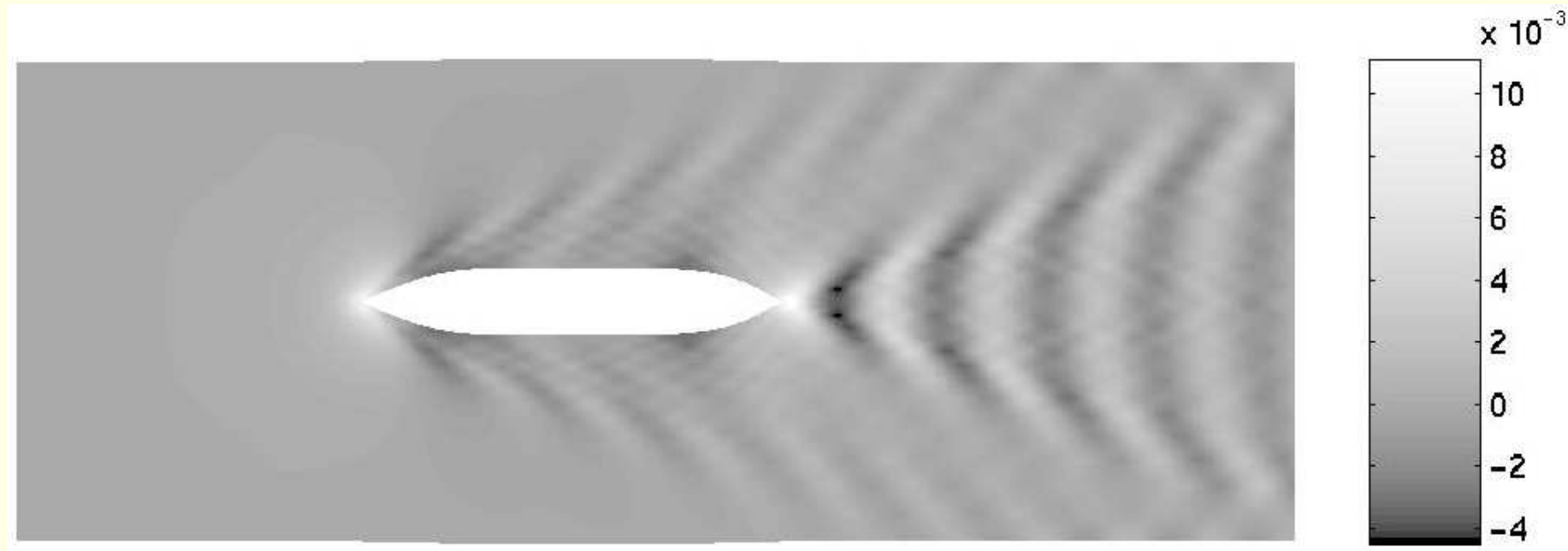


$\theta = 0, \pi/8, \pi/4, 3\pi/4, \pi/2$ (top down), $Fn = 0.4$, $\hat{\alpha} = 0.05$, $\mu = 1$, $\lambda = 1$.

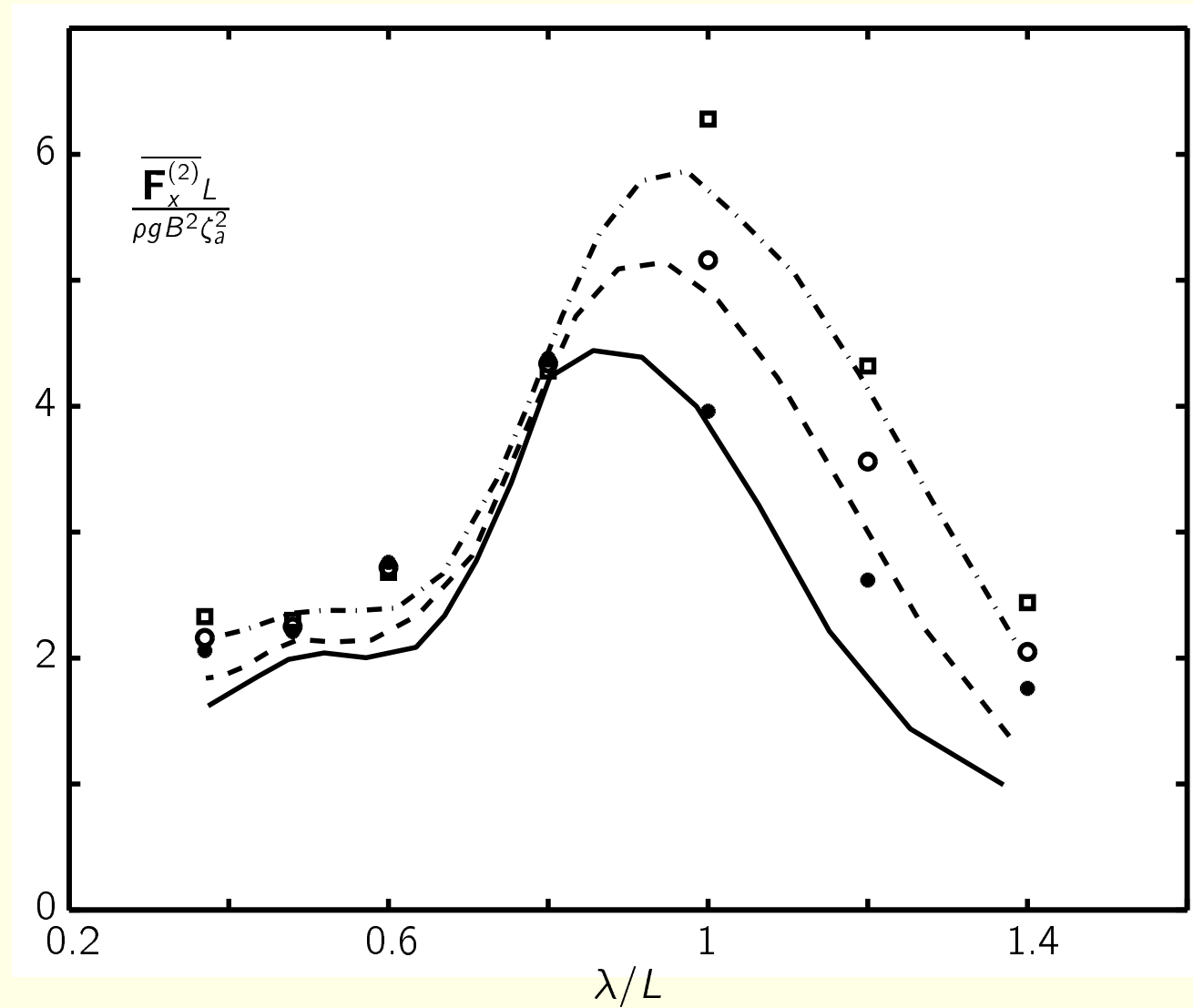
Hull paneling of LNG carrier for Froude number 0.2.



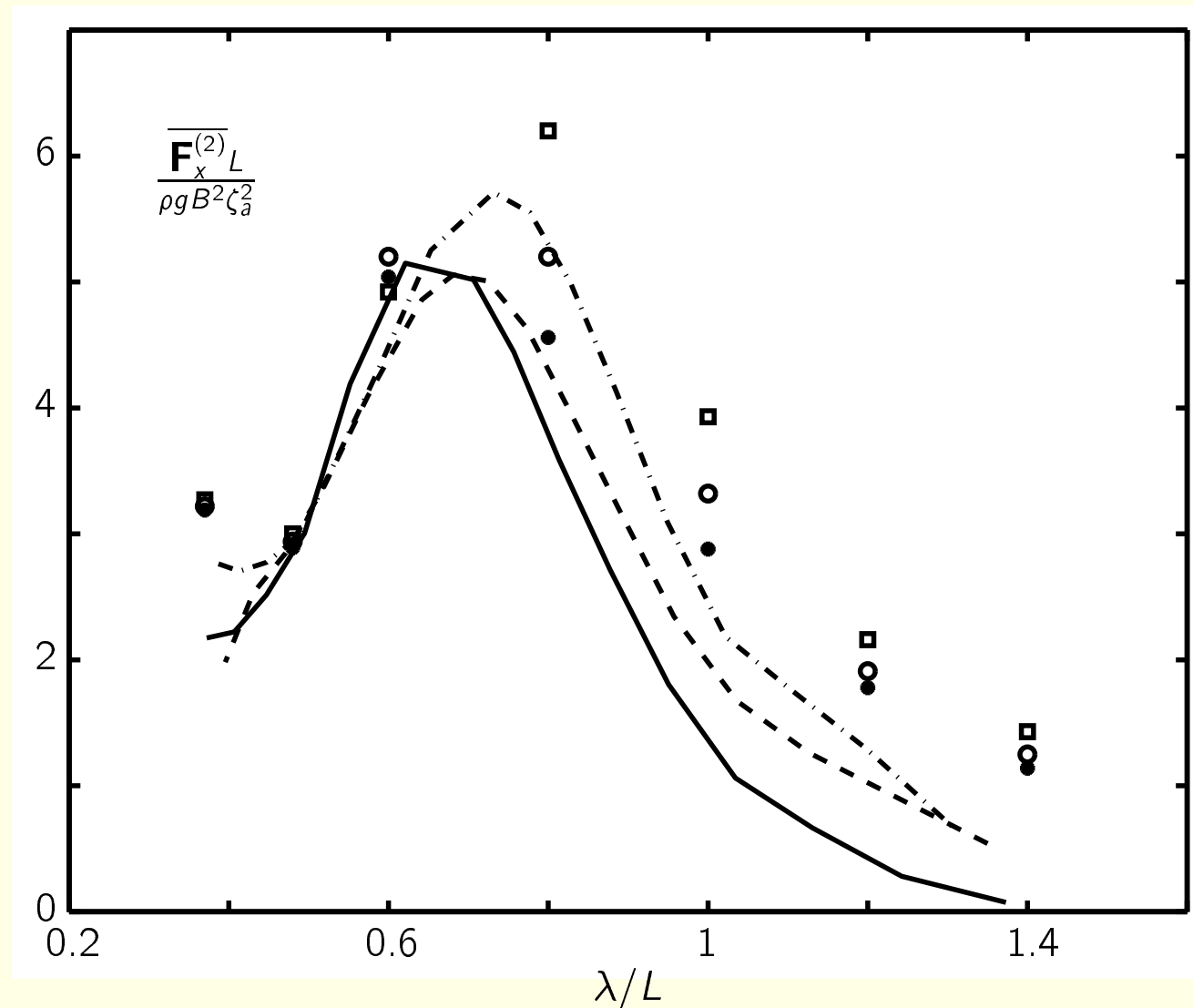
Steady wave pattern for Froude number 0.2



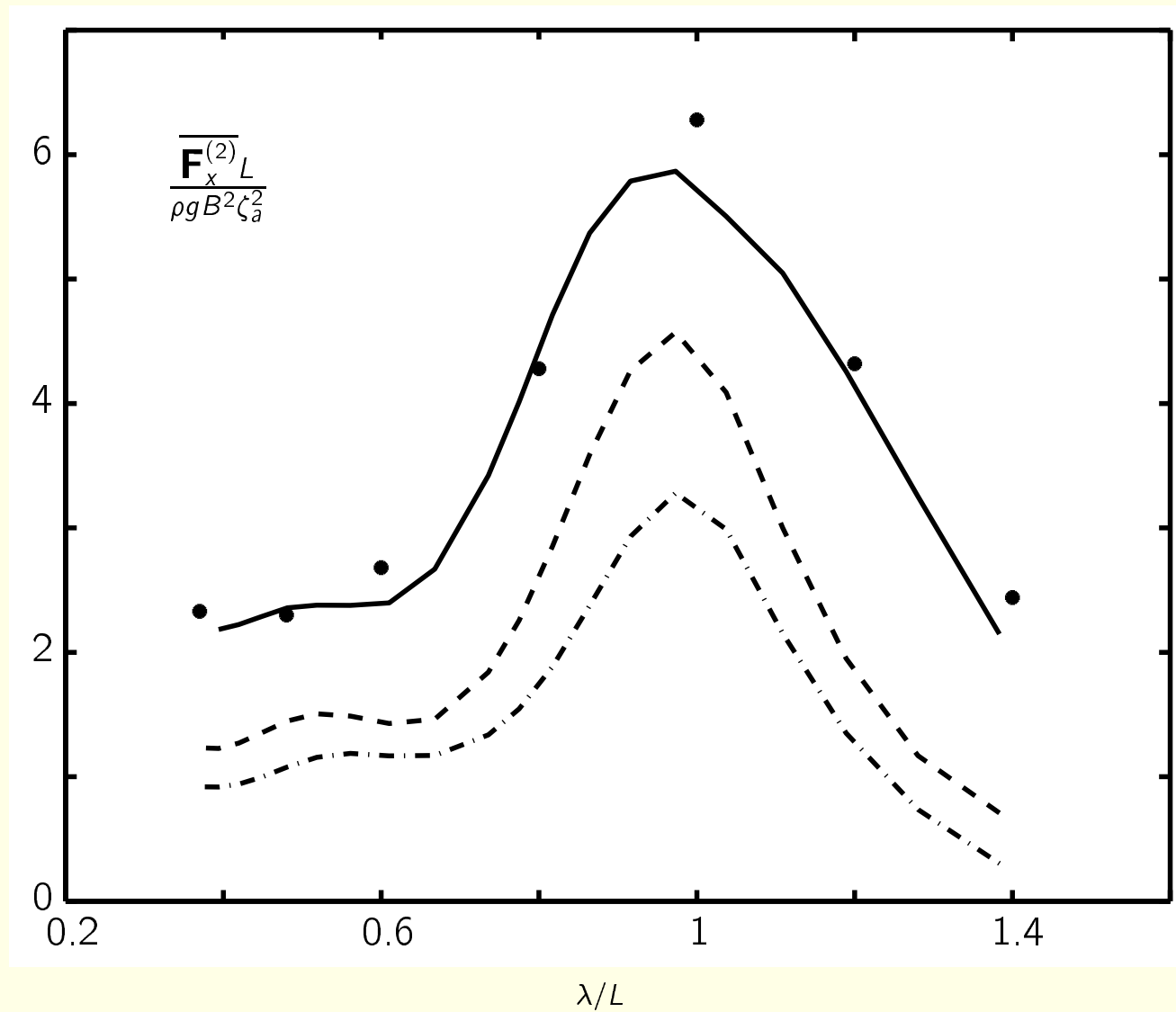
Added resistance $F_n = 0.2, 0.17, 0.14$



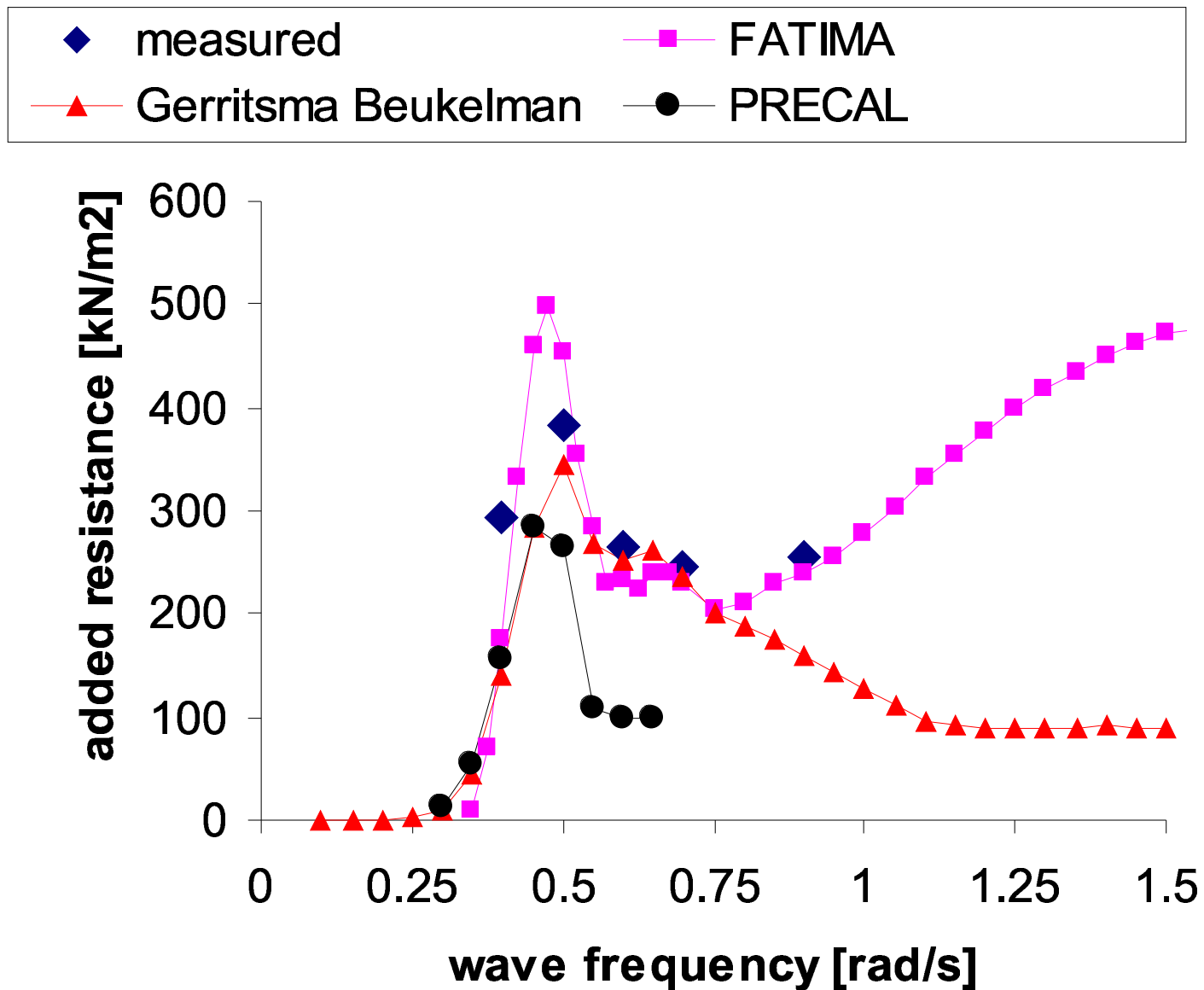
Added resistance (bow-quartering)



Added resistance with different steady flow



Results cruise carrier



Comparison with asymptotic results

