

Ray Method for the deflection of an inhomogeneous FFP

The Ray Method for the deflection of a Floating Flexible Platform in
Short waves.

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Ray Method for the deflection of an inhomogeneous FFP

Ray hypothesis:

For propagating and evanescent modes (e.g. for deep water **3**) we obtain:

- Equations for the phase and amplitude functions for inhomogeneous thin plate on water with depth (in)finite.
- Insufficient (initial) boundary conditions (**2**).

Canonical Problem ??

- Homogeneous half-plane problem
- Exact solution by means of differential-integral formulation.

Formulation

Dimensionless and harmonic $\Phi(\vec{x}, t) = \phi(\vec{x}) e^{-i\omega t}$:

$$\vec{x}' = \frac{\vec{x}}{L}, \quad h' = \frac{h}{L}, \quad K = \frac{\omega^2 L}{g}, \quad \mu = \frac{m\omega^2}{\rho g}, \quad \mathcal{D} = \frac{DK^4}{L^4 \rho g}$$

$$\Delta\Phi = 0 \quad \text{in the fluid,}$$

$$-K\phi + \frac{\partial\Phi}{\partial z} = 0 \quad \text{at } z = 0 \text{ and } (x, y) \in \mathcal{F}$$

$$\left\{ \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \left(\frac{\mathcal{D}(x, y)}{K^4} \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \right) + \frac{m(x, y)}{\rho g} \frac{\partial^2}{\partial t^2} + 1 \right\} \frac{\partial\phi}{\partial z} - K\phi = 0$$

at $z = 0$ and $(x, y) \in \mathcal{P}$

Edge conditions

Consider the case with $D(x, y)$ and its normal derivative constant along the edge.

$$\frac{\partial^2 w}{\partial n^2} + \nu \frac{\partial^2 w}{\partial s^2} = 0$$

and

$$\frac{\partial^3 w}{\partial n^3} + (2 - \nu) \frac{\partial^3 w}{\partial n \partial s^2} = 0$$

where

$$w = \frac{i}{\omega L} \phi_z$$

The incident field

In the water region we have:

$$\phi^{inc}(\vec{x}) = \frac{g\zeta_{\infty}}{i\omega} \frac{\cosh(k_0(z+h))}{\cosh(k_0h)} \exp\{ik_0(x\cos\beta + y\sin\beta)\}$$

with for finite depth:

$$k_0 \tanh(k_0h) = K$$

and infinite depth:

$$K = k_0 = \omega^2 L / g$$

Underneath the platform

For $K \gg 1$ *Ray Ansatz*:

Assume n-modes.

For $h = \infty$ each mode is written as:

$$\phi(\vec{x}, K) = \sum_n \alpha_n(\vec{x}, K) e^{iKS_n(\vec{x})}$$

with:

$$\alpha_n(\vec{x}, K) = \sum_{j=0}^N \frac{\alpha_{n,j}(\vec{x})}{(iK)^j} + o((iK)^{-N})$$

The Laplace equation yields for $z \leq 0$:

$$O(K^2) : \nabla_3 S \cdot \nabla_3 S = 0,$$

and

$$O(K^1) : 2\nabla_3 \alpha_0 \cdot \nabla_3 S + \alpha_0 \Delta_3 S = 0$$

At the platform

At $z = 0$:

$$O(K^1) : \{ \mathcal{D}(x, y)(S_x^2 + S_y^2)^2 - \mu(x, y) + 1 \} iS_z = 1$$

and $O(K^0)$:

$$\alpha_0 \mathcal{D} \left[\frac{\partial}{\partial z} (S_x^2 + S_y^2)^2 + 2S_z \left\{ \frac{\partial}{\partial x} S_x (S_x^2 + S_y^2) + \frac{\partial}{\partial y} S_y (S_x^2 + S_y^2) \right\} \right] +$$

$$\alpha_{0z} \{ \mathcal{D}(x, y)(S_x^2 + S_y^2)^2 - \mu(x, y) + 1 \} +$$

$$(4\mathcal{D}\nabla\alpha_0 \cdot \nabla S + 2\alpha\nabla\mathcal{D} \cdot \nabla S)S_z(S_x^2 + S_y^2) = 0$$

At the platform

Combine the equations in the fluid and at the plate:

With $r = iS_z$ we get

$$(\mathcal{D}(x, y)r^4 - \mu(x, y) + 1)r = 1$$

in the deep water case and

$$(\mathcal{D}(x, y)r^4 - \mu(x, y) + 1)r \tanh rh = 1$$

in the finite water depth case

combined with:

$$S_x^2 + S_y^2 = r^2$$

This resembles the *eikonal* equation in acoustics.

Characteristics

For constant values of μ :

$$\frac{dx}{d\sigma} = \mathcal{F} S_x, \quad \frac{dy}{d\sigma} = \mathcal{F} S_y, \\ \frac{dS_x}{d\sigma} = -\mathcal{D}_x r^5, \quad \frac{dS_y}{d\sigma} = -\mathcal{D}_y r^5, \quad \frac{dS}{d\sigma} = \mathcal{F} r^2$$

with:

$$\mathcal{F} = (5\mathcal{D}r^4 - \mu + 1)/r$$

The amplitude equation becomes along the characteristic:

$$\frac{d\alpha_0}{d\sigma} = -\alpha_0 M\{S\}$$

with:

$$M\{S\}(x, y) = \frac{\frac{dr}{d\sigma} \left\{ 16r^4 \mathcal{D} - \frac{1}{r} \right\} - \mathcal{F} (S_{xx} + S_{yy}) (4\mathcal{D}r^5 + 1) + 4r^4 \frac{\partial \mathcal{D}}{\partial \sigma}}{8\mathcal{D}r^5 + 2}$$

Boundary conditions

So far so good.

Three modes, two boundary conditions (at $z = 0$).

End of Story ??



Canonical Problem

Differential-Integral formulation:

$$\begin{aligned} & 4\pi \left(1 - \mu(x, y) + \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \frac{\mathcal{D}(x, y)}{K^4} \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right) \right) w(x, y) \\ & + K \int_{\mathcal{P}} \mathcal{G}(x, y; \xi, \eta) \left(\mu(\xi, \eta) - \left(\frac{\partial^2}{\partial \xi^2} + \frac{\partial^2}{\partial \eta^2} \right) \frac{\mathcal{D}(\xi, \eta)}{K^4} \left(\frac{\partial^2}{\partial \xi^2} + \frac{\partial^2}{\partial \eta^2} \right) \right) \\ & \times w(\xi, \eta) \, dS = 4\pi \zeta^\infty \exp\{ik_0(x \cos \beta + y \sin \beta)\} \end{aligned}$$

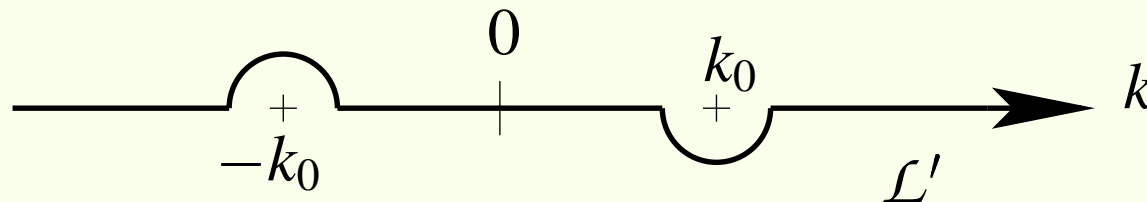
Green's Function

Green's function in 2-D at $z = \zeta = 0$ (1-D platform):

$$\mathcal{G}(x; \xi) = - \int_{\mathcal{L}'} \frac{\cosh kh}{k \sinh kh - K \cosh kh} e^{ik(x-\xi)} dk$$

Green's function in 3-D at $z = \zeta = 0$ (2-D platform):

$$\mathcal{G}(x, y; \xi, \eta) = -2 \int_0^\infty \frac{k \cosh kh}{k \sinh kh - K \cosh kh} J_0(kR) dk$$



Geometrical-Optics *Ansatz*

Homogeneous platform:

$$w(x, y) = \sum_n a_n \exp \{ i \kappa_n x + i k_0 y \sin \beta \}$$

for

$$0 \leq \beta \leq \beta_{cr} < \frac{\pi}{2}$$

Geometrical-Optics

We obtain:

$$\sum_n a_n \left(\frac{\mathcal{D}}{K^4} \kappa^{(n)4} - (\mu - 1) \right) e^{i\kappa_n x} = \zeta_\infty e^{ik_0 x \cos \beta} +$$

$$+ i \sum_n a_n \frac{K}{4\pi} \left(\frac{\mathcal{D}}{K^4} \kappa^{(n)4} - \mu \right) \int_{\mathcal{L}'} \frac{\cosh kh}{k \sinh kh - K \cosh kh}$$

$$\left(\frac{e^{ix\sqrt{k^2 - k_0^2 \sin^2 \beta}}}{\sqrt{k^2 - k_0^2 \sin^2 \beta} - \kappa_n} - \frac{e^{-ix\sqrt{k^2 - k_0^2 \sin^2 \beta}}}{\sqrt{k^2 - k_0^2 \sin^2 \beta} + \kappa_n} \right) \frac{k dk}{\sqrt{k^2 - k_0^2 \sin^2 \beta}}$$

with

$$\kappa^{(n)2} = \kappa_n^2 + k_0^2 \sin^2 \beta$$

The integral

For $\beta = 0$ we have:

$$i \sum_n a_n \frac{K}{2\pi} \left(\frac{\mathcal{D}}{K^4} \kappa^{(n)4} - \mu \right) \int_{\mathcal{L}'} \frac{\cosh kh}{k \sinh kh - K \cosh kh} \left(\frac{e^{ixk}}{k - \kappa_n} - \frac{e^{-ixk}}{k + \kappa_n} \right) dk$$

If $\Im \kappa_n > 0$ then contribution of first term,

If $\Im \kappa_n < 0$ then contribution of second term.

Dispersion Relation

We close the contour either in the upper or lower half-plane

This results in the dispersion relation for $\kappa^{(n)}$:

$$\left(\frac{\mathcal{D}}{K^4} \kappa^4 - \mu + 1 \right) \kappa \tanh \kappa h = K$$

we take into account one real (travelling wave)

and $N + 2$ complex solutions (evanescent waves)

$N + 3$ modes and **TWO** boundary conditions

Boundary conditions

For the amplitudes we obtain at $x = 0$

$$-\sum_{n=1}^3 (\kappa_n^2 + \nu k_0^2 \sin^2 \beta) a_n = 0$$

and

$$-i \sum_{n=1}^3 \kappa_n (\kappa_n^2 + (2 - \nu) k_0^2 \sin^2 \beta) a_n = 0$$

$N + 1$ missing relation

From the pole at $k = k_0$ we get a **third** relation:

$$\sum_{n=0}^{N+2} \frac{K \left(\frac{\mathcal{D}\kappa^{(n)4}}{K^4} - \mu \right) k_0 a_n}{(K(1 - Kh) + k_0^2 h) \cos \beta (\kappa_n - k_0 \cos \beta)} + \zeta_\infty = 0$$

and for $i = 1, \dots, N$:

$$\sum_{n=0}^{N+2} \frac{K \left(\frac{\mathcal{D}\kappa^{(n)4}}{K^4} - \mu \right) k_i a_n}{(K(1 - Kh) + k_i^2 h) \sqrt{k_i^2 - k_0^2 \sin^2 \beta} \left(\kappa_n - \sqrt{k_i^2 - k_0^2 \sin^2 \beta} \right)} = 0$$

Exact solution for a Strip

The same approach for the Strip with width L :

$$w(x, y) = \sum_{n=0}^N (a_n \exp\{i\kappa_n x\} + b_n \exp\{-i\kappa_n(x - L)\}) \exp\{ik_0 y \sin \beta\}$$

Moving Rigid Strip ($\beta = 0$)

The equations of motion give **two** equations

$$\sum_{n=1}^N \left[\frac{a_n + b_n}{i\kappa_n} (e^{i\kappa_n l} - 1) \right] + \left[\frac{KM}{\rho} - l \right] \frac{w}{\zeta_\infty} = 0$$

and

$$\sum_{n=1}^N (a_n - b_n) \left[\frac{1}{\kappa_n^2} (e^{i\kappa_n l} - 1) + \frac{1}{i\kappa_n} (e^{i\kappa_n l} + 1) \right] + \left[\frac{KI}{\rho} - \frac{l^3}{12} \right] \frac{\theta}{\zeta_\infty} = 0$$

where w and θ are the heave and pitch amplitude.

The pole analysis leads to **$2N$** equations:



Moving Rigid Strip

$$k_0 \sum_{n=1}^N \left[\frac{a_n}{\kappa_n - k_0} - \frac{b_n e^{i\kappa_n l}}{\kappa_n + k_0} \right] + \frac{1}{\zeta^\infty} \left[w + \theta \left(\frac{1}{ik_0} - \frac{l}{2} \right) \right] = Kh - 1 - \frac{k_0^2 h}{K}$$

and

$$k_0 \sum_{n=1}^N \left[\frac{-a_n e^{i\kappa_n l}}{\kappa_n + k_0} + \frac{b_n}{\kappa_n - k_0} \right] + \frac{1}{\zeta^\infty} \left[w - \theta \left(\frac{1}{ik_0} - \frac{l}{2} \right) \right] e^{ik_0 l} = 0$$

For $i = 1, \dots, N-1$ we obtain:

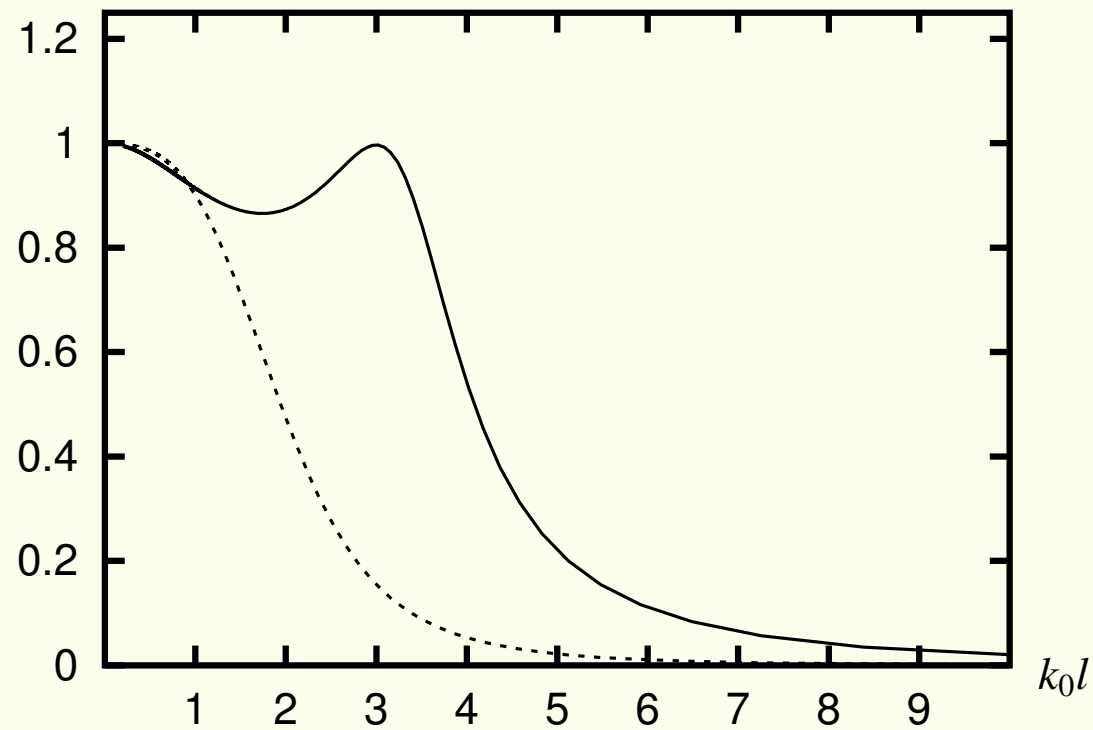
$$k_i \sum_{n=1}^N \left[\frac{a_n}{\kappa_n - k_i} - \frac{b_n e^{i\kappa_n l}}{\kappa_n + k_i} \right] + \frac{1}{\zeta^\infty} \left[w + \theta \left(\frac{1}{ik_i} - \frac{l}{2} \right) \right] = 0$$

and

$$k_i \sum_{n=1}^N \left[\frac{-a_n e^{i\kappa_n l}}{\kappa_n + k_i} + \frac{b_n}{\kappa_n - k_i} \right] + \frac{1}{\zeta^\infty} \left[w - \theta \left(\frac{1}{ik_i} - \frac{l}{2} \right) \right] e^{ik_i l} = 0$$

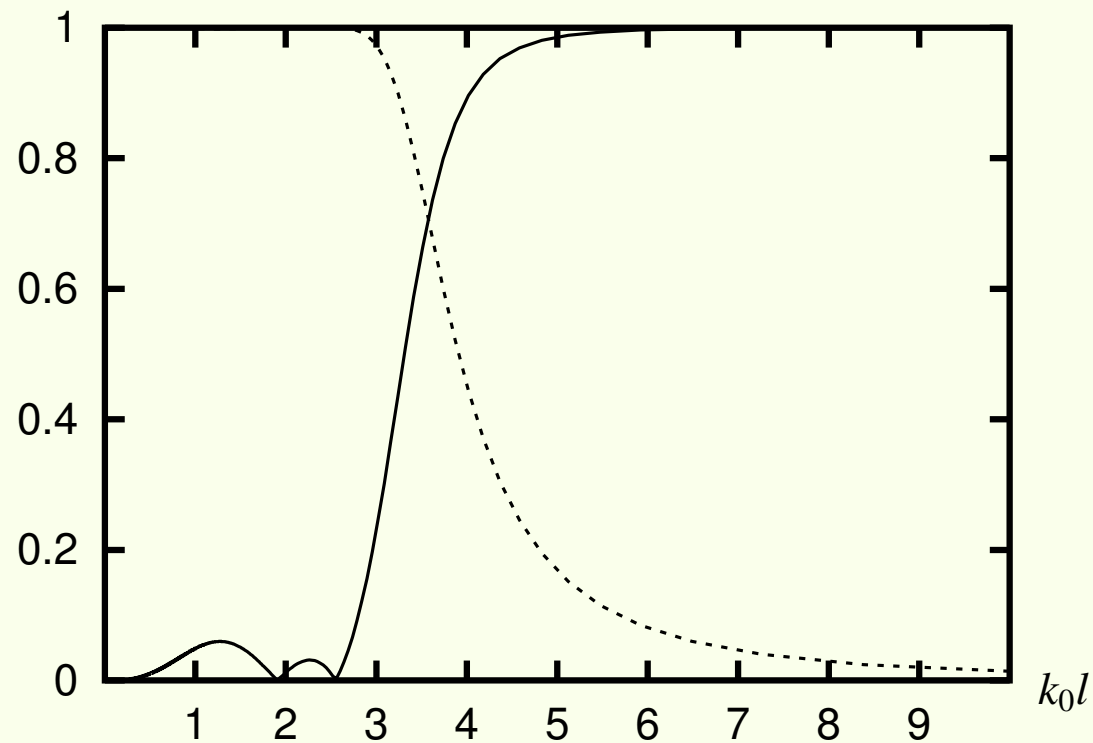


Heave and Pitch amplitudes



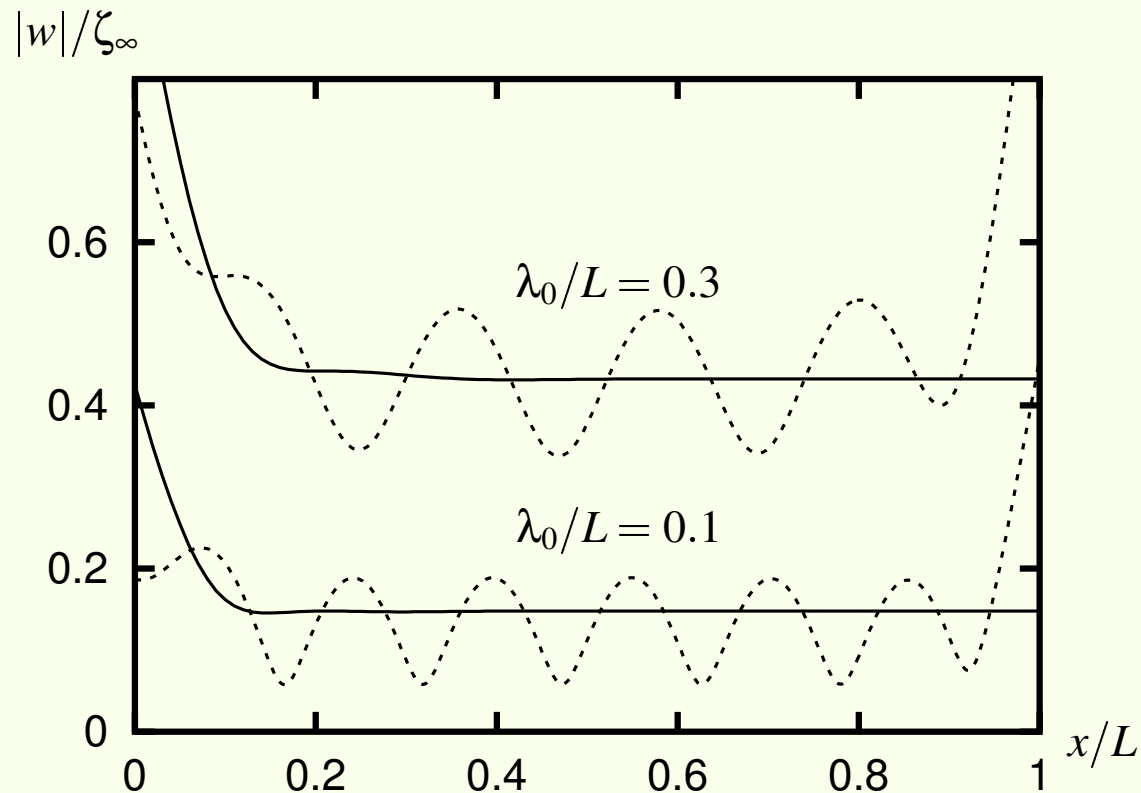
Amplitude of the heave, — w/ζ^∞ and pitch motion, ... $\theta/(k_0 \zeta^\infty)$

Reflection and Transmission coefficients



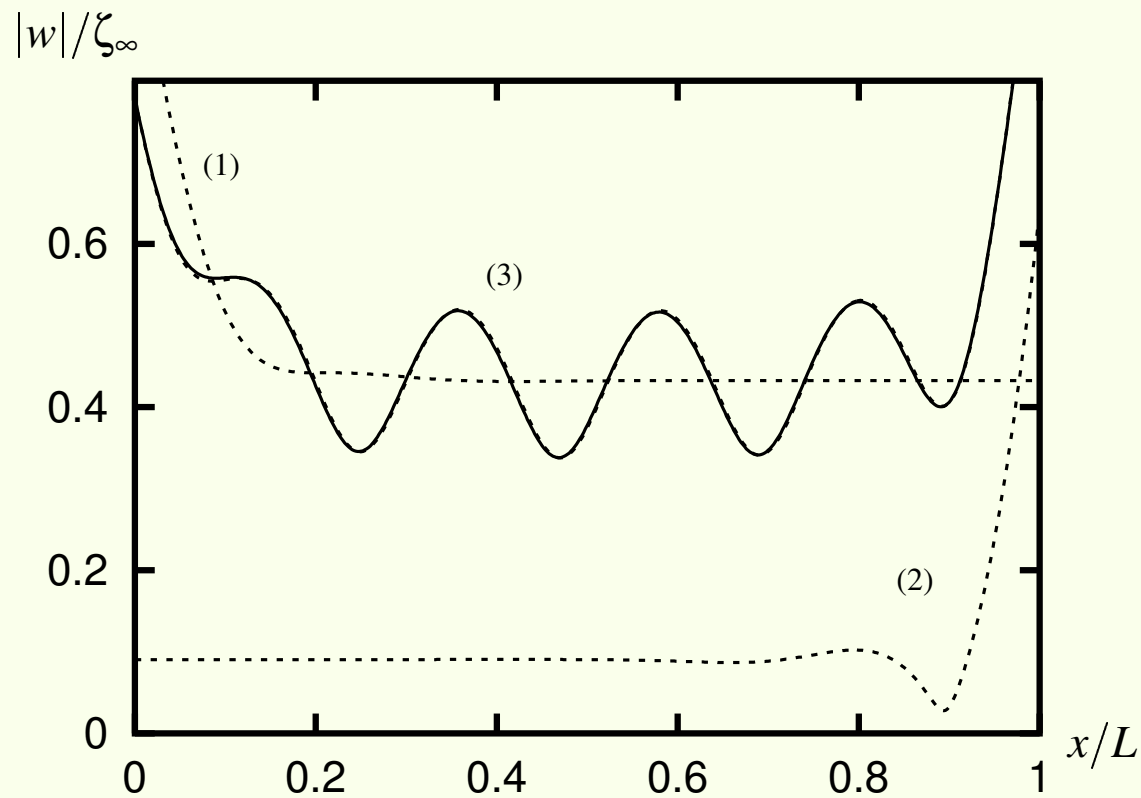
___ reflection and ... transmission coefficient.

Flexible half-plane and strip



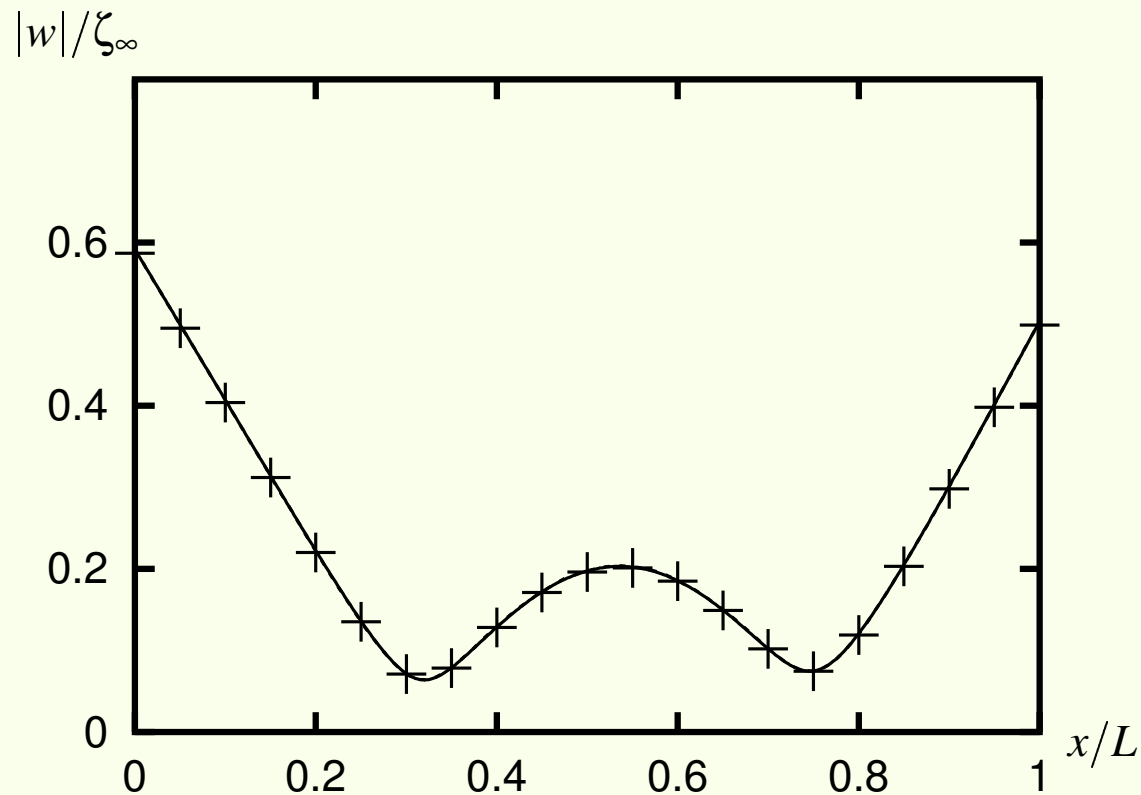
Asymptotic results for finite and semi-infinite (dotted) platform. Example with parameters $D/\rho g = 1.23 * 10^{-5} * L^4$, $h/L = 1/3$ and $\beta = 0$

Multiple reflection



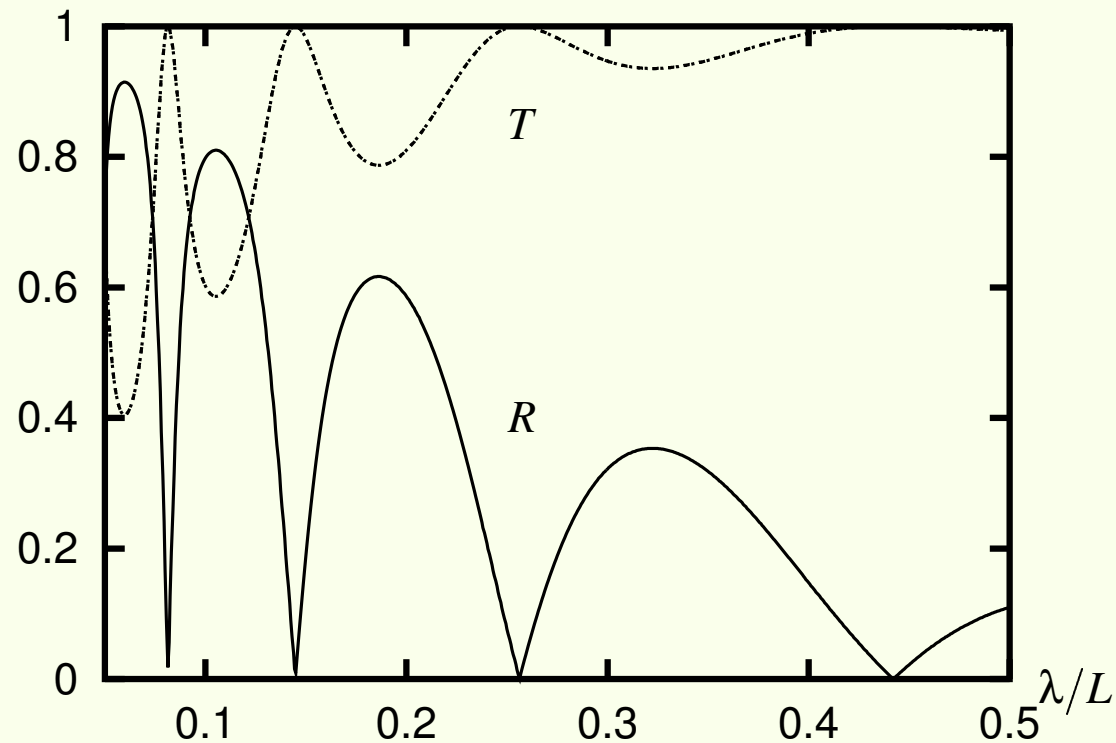
Multiple reflection $\lambda_0/L = 0.3$,

Comparison with Takagi



Comparison with the asymptotic results of Takagi for $\lambda_0/L = 0.278$ and $D/\rho g = 1.74 * 10^{-3} * L^4$, $h/L \approx 1/3$ and $\beta = 0$.

Reflection and Transmission Coefficient



Reflection and transmission coefficients $D/\rho g = 1.23 * 10^{-5} * L^4$, $h/L = 1/3$ and $\beta = 0$.

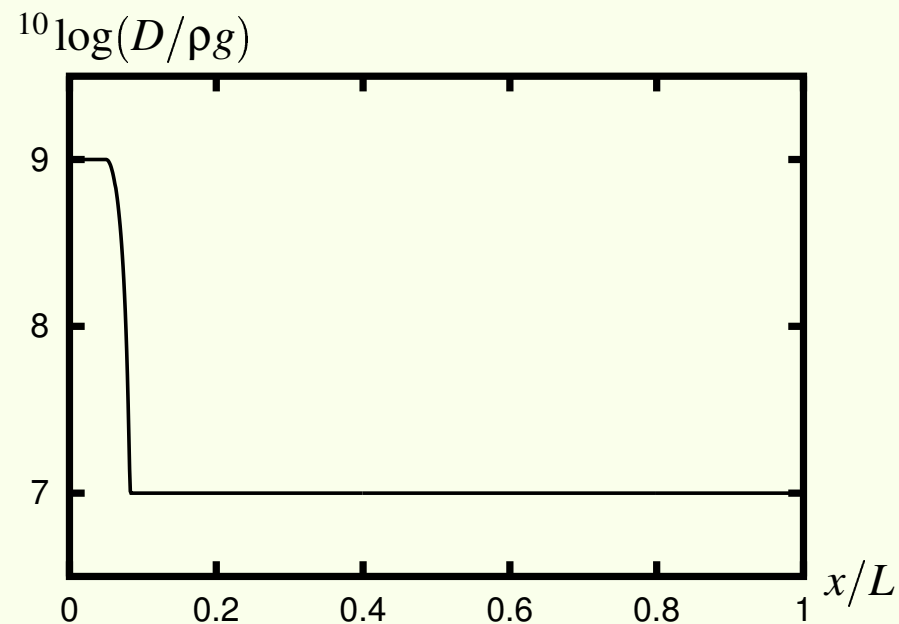
Application of the Ray Method

Inhomogeneous 2-D case with $D/(\rho g) = d(x)$:

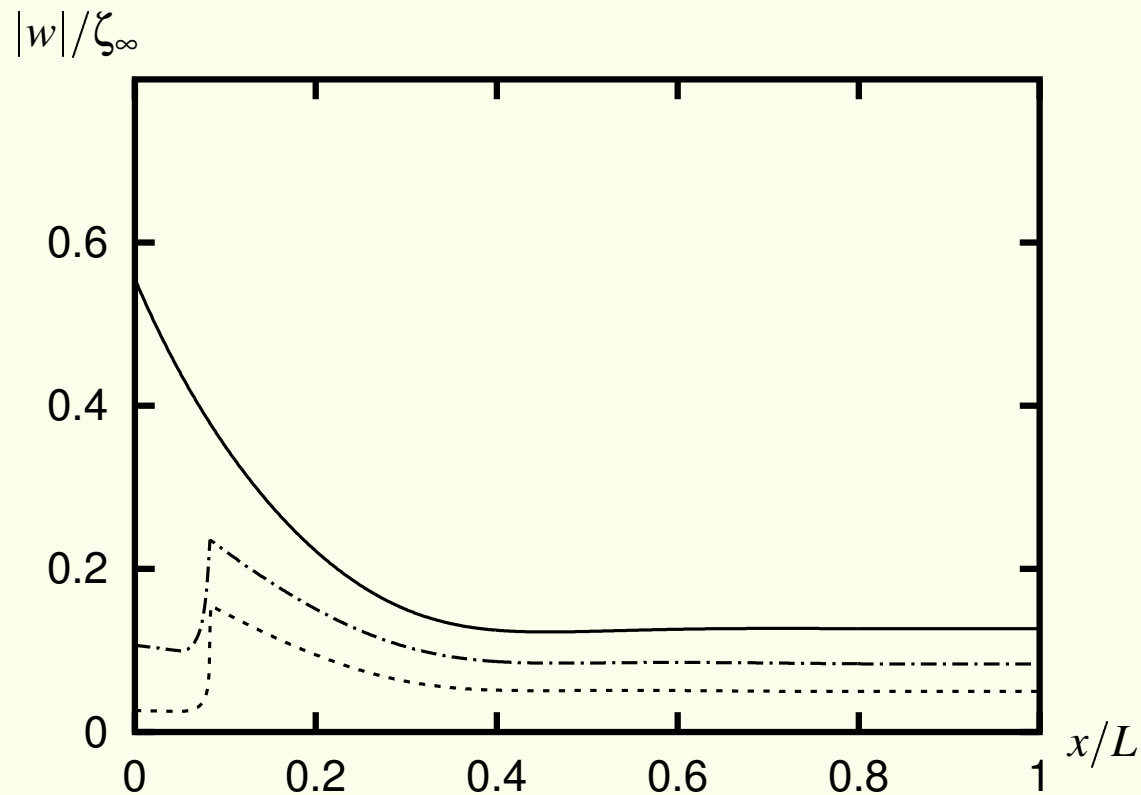
$$d = d^{(1)} = 10^9 \quad \text{for } 0 \leq x < 15 \text{ m}$$

$$d = \{d^{(1)} + d^{(2)} + (d^{(1)} - d^{(2)}) \cos((x - 15)\pi/10)\} / 2 \quad \text{for } 15 \leq x < 25 \text{ m}$$

$$d = d^{(2)} = 10^7 \quad \text{for } 25 \leq x < \infty$$

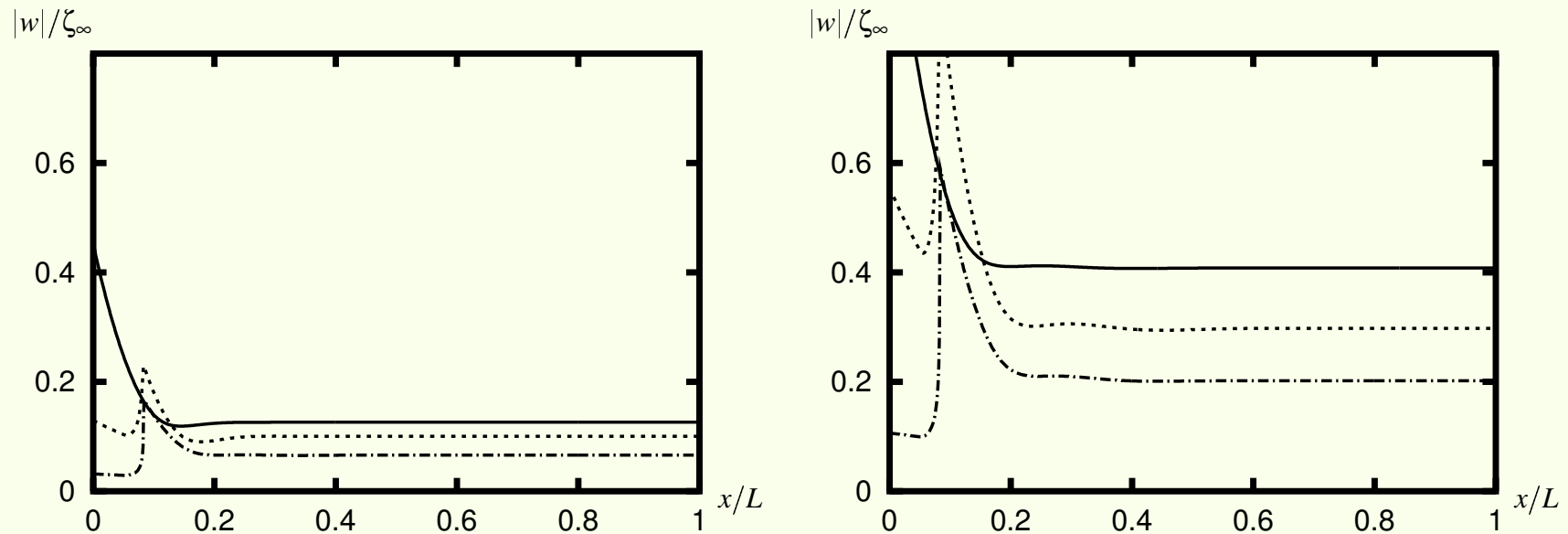


Semi infinite plate



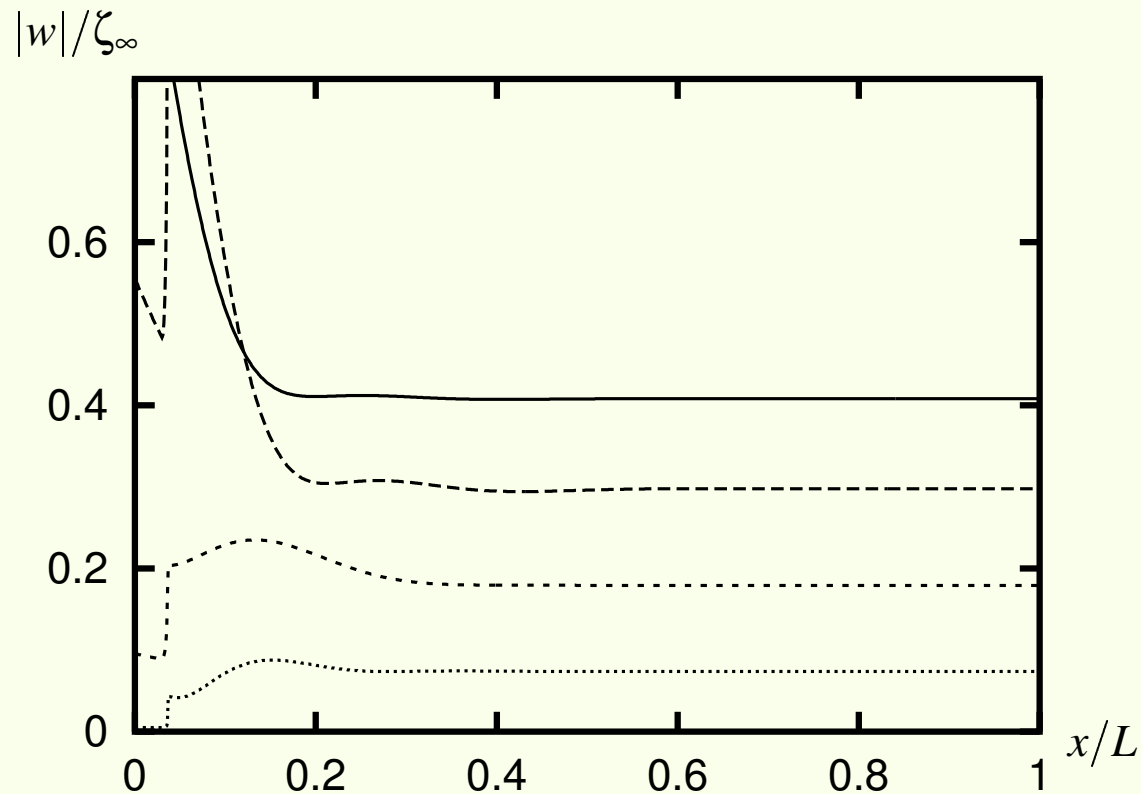
Amplitude of deflection for $d = 10^7 \text{ m}^4$ (top), and $d^{(1)} 10^9 \text{ m}^4$ (middle), 10^{11} m^4 (bottom) resp. with $d^{(2)} = 10^7 \text{ m}^4$, $\lambda_0/L = 0.3$ (with $L = 300 \text{ m}$)

Variation of wave-length



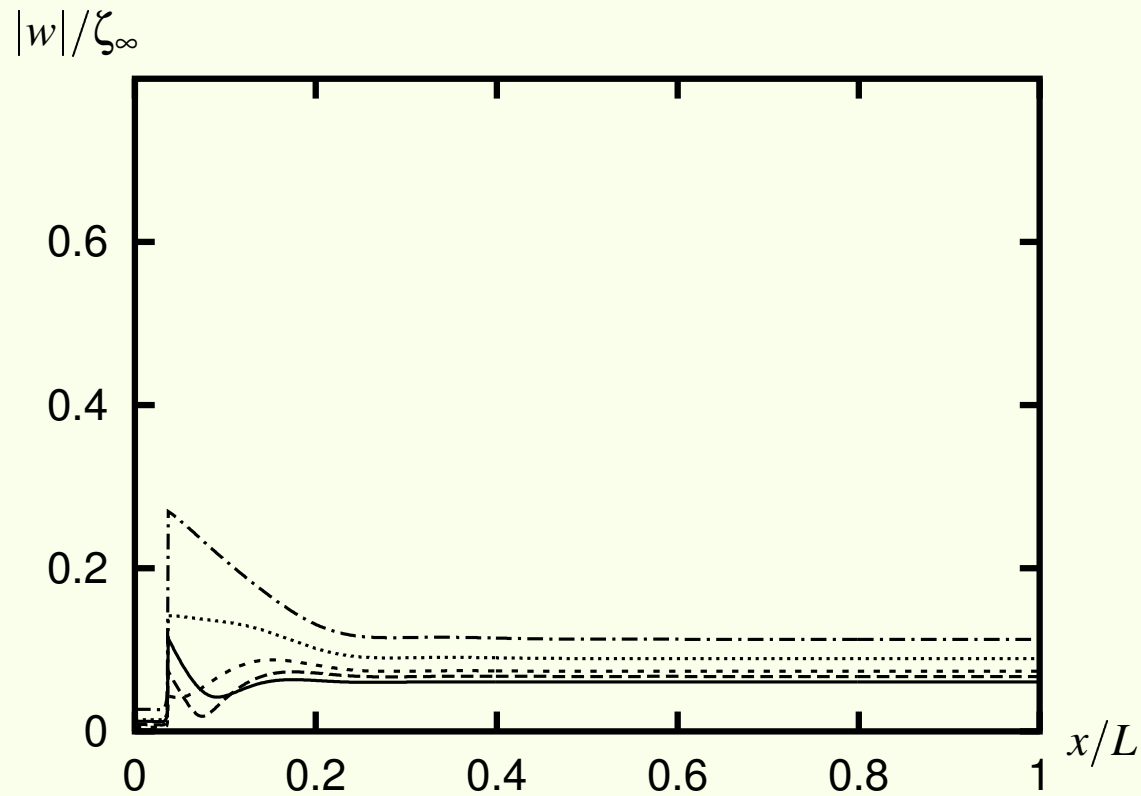
Amplitude of deflection for $d = 10^5 \text{ m}^4$ (top), and $d^{(1)} = 10^7 \text{ m}^4$ (middle), 10^9 m^4 (bottom) resp. with $d^{(2)} = 10^5 \text{ m}^4$, $\lambda_0/L = 0.1$ (left) and $\lambda_0/L = 0.3$ (right) for a semi infinite plate ($L = 300 \text{ m}$).

Extra weight at the edge



top to bottom $c = 0, d = 10^5 \text{ m}^4$; $c = 0, d^{(1)} = 10^7 \text{ m}^4$ and $d^{(2)} = 10^5 \text{ m}^4$;
 $c = 2, d = 10^5 \text{ m}^4$; $c = 2, d^{(1)} = 10^7 \text{ m}^4$ and $d^{(2)} = 10^5 \text{ m}^4$.

Variation of wave-length



top to bottom $c = 6, d^{(1)} = 10^{10} \text{ m}^4, d^{(2)} = 10^5 \text{ m}^4, \lambda_0/L = 0.5, \dots, 0.1 \text{ m}$